

REFRACTION

To be subtracted from sextant altitude (referred to as observed altitude in A.P. 3270)

R_o	Height above sea level in units of 1 000 ft.										R_o	$R = R_o \times f$				
	0	5	10	15	20	25	30	35	40	45		R_o	f	$0.9 \ 1.0 \ 1.1 \ 1.2$	R	
Sextant Altitude																
' 90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	90 90 90	
0 63 59 55	51 46 41	36 31 26	22 19 16	14 11 9	8 7 5	6 5 3	2 20 10	2 20 10	2 20 10	2 20 10	2 20 10	2 20 10	2 20 10	2 20 10	2 20 10	2 20 10
1 33 29 26	22 19 16	14 12 10	10 8 7	8 7 5	4 00 3 10	3 10 2 10	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39
2 21 19 16	14 12 10	10 8 7	8 7 5	4 00 3 10	3 10 2 10	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39
3 16 14 12	10 8 7	8 7 5	4 00 3 10	3 10 2 10	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39
4 12 11 9	8 7 5	4 00 3 10	3 10 2 10	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39	1 30 0 39
5 10 9 7	5 50 4 50	3 50 3 50	4 50 4 00	3 00 2 20	1 50 1 10	1 50 1 20	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44
6 8 10 6 50	6 50 5 50	4 50 4 00	3 00 2 20	1 50 1 10	1 50 1 20	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44
7 6 50 5 50	5 50 5 00	4 00 3 10	2 30 1 50	1 20 0 38	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44	0 38 0 44
8 6 00 5 10	4 10 3 20	3 20 2 40	2 00 1 30	1 00 0 19	0 19 0 13	0 13 0 13	0 13 0 13	0 13 0 13	0 13 0 13	0 13 0 13	0 13 0 13	0 13 0 13	0 13 0 13	0 13 0 13	0 13 0 13	0 13 0 13
9 5 20 4 30	3 40 2 50	2 50 2 10	1 40 1 10	1 10 0 35	0 35 0 03	0 27 0 53	0 27 0 53	0 27 0 53	0 27 0 53	0 27 0 53	0 27 0 53	0 27 0 53	0 27 0 53	0 27 0 53	0 27 0 53	0 27 0 53
10 4 30 3 40	2 50 2 10	2 20 1 40	1 10 0 35	0 37 0 11	0 11 0 16	0 43 0 13	0 43 0 13	0 43 0 13	0 43 0 13	0 43 0 13	0 43 0 13	0 43 0 13	0 43 0 13	0 43 0 13	0 43 0 13	0 43 0 13
12 3 30 2 50	2 10 1 40	1 40 1 10	0 34 0 09	0 09 0 14	0 14 0 37	0 00 0 23	0 23 0 44	0 23 0 44	0 23 0 44	0 23 0 44	0 23 0 44	0 23 0 44	0 23 0 44	0 23 0 44	0 23 0 44	0 23 0 44
14 2 50 2 10	1 40 1 10	0 37 0 10	0 10 0 13	0 13 0 34	0 34 0 53	0 14 0 13	0 13 0 56	0 13 0 56	0 13 0 56	0 13 0 56	0 13 0 56	0 13 0 56	0 13 0 56	0 13 0 56	0 13 0 56	0 13 0 56
16 2 20 1 40	1 20 1 10	0 43 0 15	0 15 0 08	0 31 0 52	0 52 0 08	0 27 0 14	0 27 0 20	0 27 0 20	0 27 0 20	0 27 0 20	0 27 0 20	0 27 0 20	0 27 0 20	0 27 0 20	0 27 0 20	0 27 0 20
18 1 50 1 20	0 49 0 23	0 02 0 26	0 26 0 46	0 10 0 46	0 46 0 22	0 39 0 15	0 39 0 24	0 39 0 24	0 39 0 24	0 39 0 24	0 39 0 24	0 39 0 24	0 39 0 24	0 39 0 24	0 39 0 24	0 39 0 24
20 1 12 0 44	+0 19 0 06	-0 28 0 48	-0 48 0 09	-0 27 0 17	0 17 0 42	-1 58 0 24	-1 58 0 30	-1 58 0 30	-1 58 0 30	-1 58 0 30	-1 58 0 30	-1 58 0 30	-1 58 0 30	-1 58 0 30	-1 58 0 30	-1 58 0 30
25 0 34 +0 10	-0 13 0 37	-0 36 0 55	-0 55 0 14	-0 32 0 32	0 32 0 51	-2 21 0 21	-2 21 0 49	-2 21 0 49	-2 21 0 49	-2 21 0 49	-2 21 0 49	-2 21 0 49	-2 21 0 49	-2 21 0 49	-2 21 0 49	-2 21 0 49
30 +0 06 -0 16	-0 37 0 59	-0 59 0 17	-0 17 0 33	-0 51 0 51	0 51 0 27	-2 37 0 27	-2 37 0 51	-2 37 0 51	-2 37 0 51	-2 37 0 51	-2 37 0 51	-2 37 0 51	-2 37 0 51	-2 37 0 51	-2 37 0 51	-2 37 0 51
35 -0 18 -0 37	-0 58 0 37	-0 16 0 34	-0 34 0 49	-0 26 0 26	0 26 0 22	-2 49 0 24	-2 49 0 30	-2 49 0 30	-2 49 0 30	-2 49 0 30	-2 49 0 30	-2 49 0 30	-2 49 0 30	-2 49 0 30	-2 49 0 30	-2 49 0 30
40 -0 53 -0 14	-0 31 0 47	-0 47 0 23	-0 23 0 18	-0 18 0 18	0 18 0 13	-2 59 0 59	-2 59 0 13	-2 59 0 13	-2 59 0 13	-2 59 0 13	-2 59 0 13	-2 59 0 13	-2 59 0 13	-2 59 0 13	-2 59 0 13	-2 59 0 13
45 -1 10 -1 28	-1 44 0 44	-1 59 0 25	-2 15 0 15	-2 28 0 28	-2 43 0 24	-2 28 0 28	-2 28 0 28	-2 28 0 28	-2 28 0 28	-2 28 0 28	-2 28 0 28	-2 28 0 28	-2 28 0 28	-2 28 0 28	-2 28 0 28	-2 28 0 28
50 -1 40 -1 53	-2 09 0 53	-2 24 0 24	-2 24 0 38	-2 38 0 28	-2 52 0 24	-2 38 0 38	-2 38 0 38	-2 38 0 38	-2 38 0 38	-2 38 0 38	-2 38 0 38	-2 38 0 38	-2 38 0 38	-2 38 0 38	-2 38 0 38	-2 38 0 38
55 -2 33 -2 18	-2 33 0 23	-2 46 0 18	-2 46 0 23	-2 46 0 26	-3 01 0 21	-3 12 0 25	-3 25 0 25	-3 25 0 25	-3 25 0 25	-3 25 0 25	-3 25 0 25	-3 25 0 25	-3 25 0 25	-3 25 0 25	-3 25 0 25	-3 25 0 25
60 -2 53 -3 07	-3 07 0 19	-2 53 0 53	-2 53 0 07	-2 53 0 31	-3 42 0 31	-3 53 0 31	-3 31 0 31	-3 31 0 31	-3 31 0 31	-3 31 0 31	-3 31 0 31	-3 31 0 31	-3 31 0 31	-3 31 0 31	-3 31 0 31	-3 31 0 31
Temperature in °C.																
f																
Temperature in °C.																
0.9 +47	+36	+27	+18	+10	+3	-5	-13									
1.0 +26	+16	+6	-4	-13	-22	-31	-40									
1.1 +5	-5	-15	-25	-36	-46	-57	-68									
1.2 -16	-25	-36	-46	-58	-71	-83	-95									
	-37	-45	-56	-67	-81	-95										
f																
f																
Temperature in °C.																
0.9 +47	+36	+27	+18	+10	+3	-5	-13									
1.0 +26	+16	+6	-4	-13	-22	-31	-40									
1.1 +5	-5	-15	-25	-36	-46	-57	-68									
1.2 -16	-25	-36	-46	-58	-71	-83	-95									
	-37	-45	-56	-67	-81	-95										

Choose the column appropriate to height, in units of 1 000 ft., and find the range of altitude in which the sextant altitude lies; the corresponding value of R_o is the refraction, to be subtracted from sextant altitude, unless conditions are extreme. In that case find f from the lower table, with critical argument temperature. Use the table on the right to form the refraction, $R = R_o \times f$.

CORIOLIS (Z) CORRECTION

To be applied by moving the position line a distance Z to starboard (right) of the track in northern latitudes and to port (left) in southern latitudes.

G/S KNOTS	Latitude					G/S KNOTS	Latitude				
	0°	10°	20°	30°	40°		0°	10°	20°	30°	40°
150 0 1 1 2	3 3	3 4	4 4			550 0 3 5 7	9 11	12 14	14 14		
200 0 1 2 3	3 4	5 5	5 5			600 0 3 5 8	10 12	14 15	16 16		
250 0 1 2 3	4 5	6 6	6 7			650 0 3 6 9	11 13	15 16	17 17		
300 0 1 3 4	5 6	7 7	8 8			700 0 3 6 9	12 14	16 17	18 18		
350 0 2 3 5	6 7	8 9	9 9			750 0 3 7 10	13 15	17 18	19 20		
400 0 2 4 5	7 8	9 10	10 10			800 0 4 7 10	13 16	18 20	21 21		
450 0 2 4 6	8 9	10 11	12 12			850 0 4 8 11	14 17	19 21	22 22		
500 0 2 4 7	8 10	11 12	13 13			900 0 4 8 12	15 18	20 22	23 24		

STANDARD DOME
REFRACTION

To be subtracted from sextant altitude when using sextant suspension in a perspex dome.

Alt. °	Refn. ,	Alt. °	Refn. ,
10	8	50	4
20	7	60	4
30	6	70	3
40	5	80	3

This table must not be used if a calibration table is fitted to the dome, or if a flat glass plate is provided, or for non-standard domes.

BUBBLE SEXTANT ERROR

Sextant Number	Alt. °	Corr. ,

CORRECTIONS TO BE APPLIED
TO MARINE SEXTANT ALTITUDES

CORRECTION FOR DIP OF THE HORIZON
To be subtracted from sextant altitude.

Ht. Ft.	Dip ,	Ht. Ft.	Dip ,	Ht. Ft.	Dip ,	Ht. Ft.	Dip ,
0	114	437	21	968	31	1 707	41
2	137	481		1 033	31	1 792	42
6	162	527	22	1 099	32	1 880	43
12	189	575	23	1 168	33	1 970	44
21	218	625	24	1 239	34	2 061	45
31	250	677	25	1 311	35	2 155	46
43	283	731	26	1 386	36	2 251	47
58	318	787	27	1 463	37	2 349	48
75	356	845	28	1 543	38	2 449	49
93	395	906	29	1 624	39	2 551	50
114	437	968	30	1 707	40	2 655	50

CORRECTIONS

In addition to sextant error and dip, corrections are to be applied for:

- Refraction
- Semi-diameter (for the Sun and Moon)
- Parallax (for the Moon)
- Dome refraction (if applicable)

MARINE SEXTANT
ERROR

Sextant Number

Index Error

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